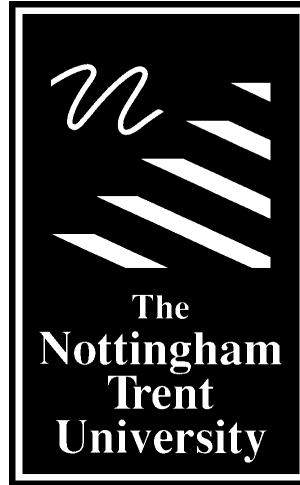




Dynamic Wetting of Structured Surfaces

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Acknowledgement

Financial support under EPSRC Grant GR/N02184/01 and Qinetiq (MOD/DERA JGS)

Overview

1. Wetting and Topography

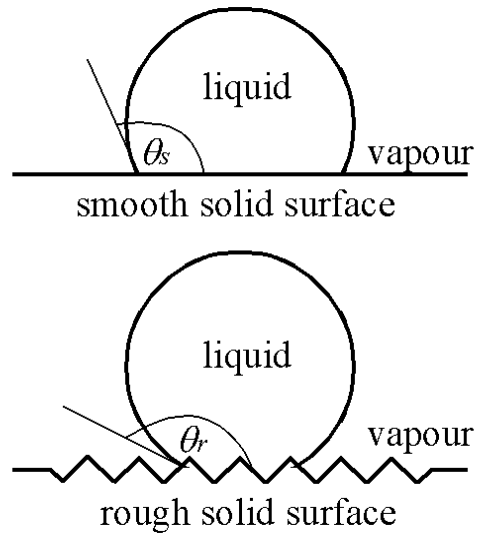
- Wenzel's Equation (*and Air Trapping*)
- Super-hydrophobicity and Super-wetting
- Tanner's Law

2. Experimental

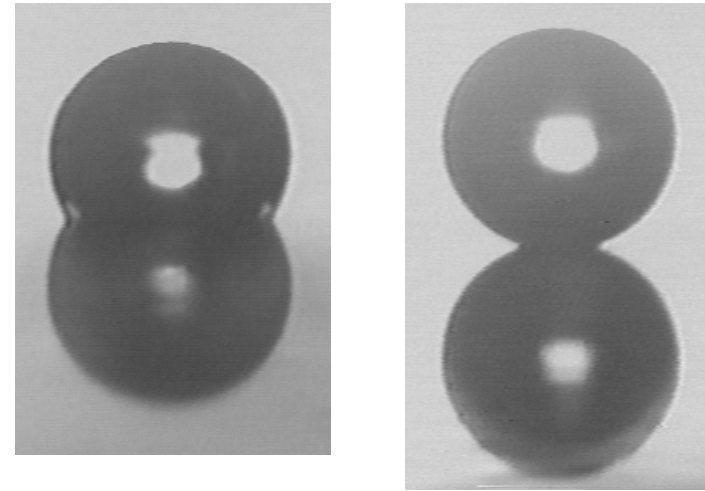
- Surface Structures - Lithographic Fabrication
- Dynamics: Super-wetting
- Equilibrium: Super-hydrophobic

3. Conclusions

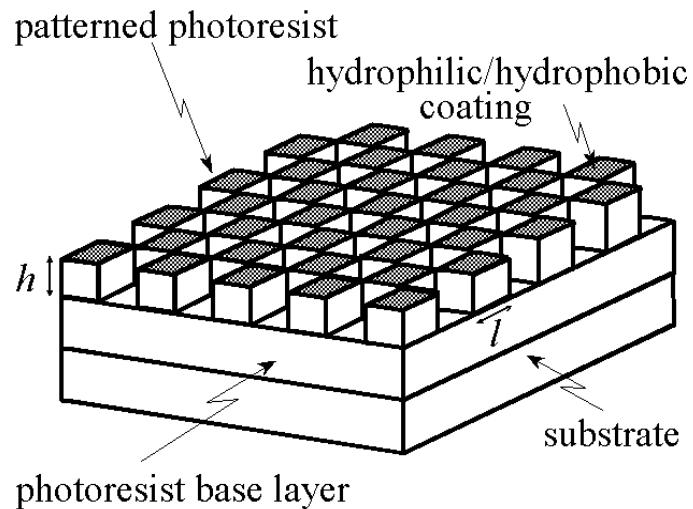
Super-Hydrophobic Surfaces



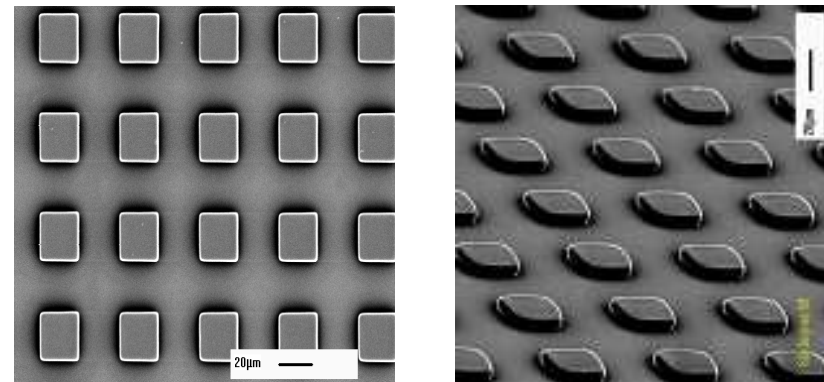
Water Drop (~ 2 mm)



Lithographic Principle

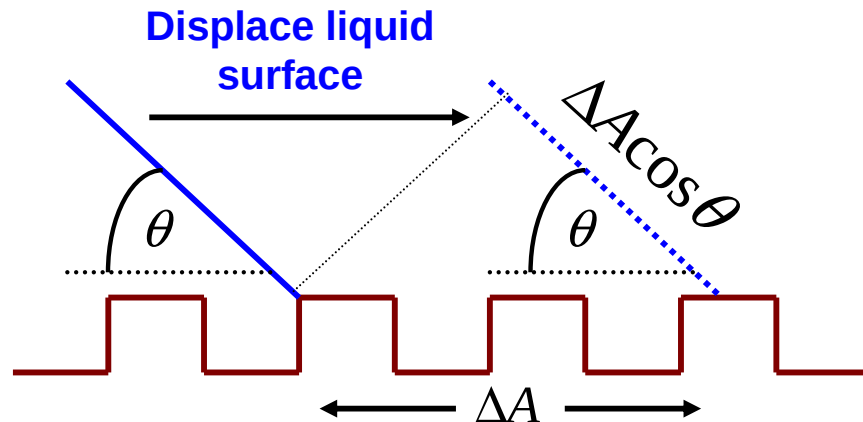


SEM Images

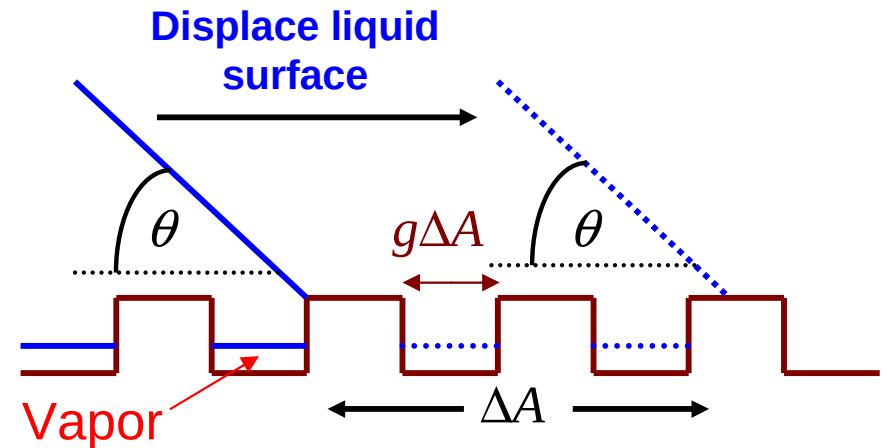


Wetting and Topography

Surface Topography



Air Trapping



Surface Free Energy Changes

$$\Delta F = (\gamma_{SL} - \gamma_{SV})r\Delta A + \gamma_{LV} \cos \theta \Delta A$$

Wenzel's Eqn

$$\cos \theta_e^R = r(\gamma_{SV} - \gamma_{SL}) / \gamma_{LV} = r \cos \theta_e^S$$

$$r = \Delta A_{\text{true}} / \Delta A = \text{roughness factor}$$

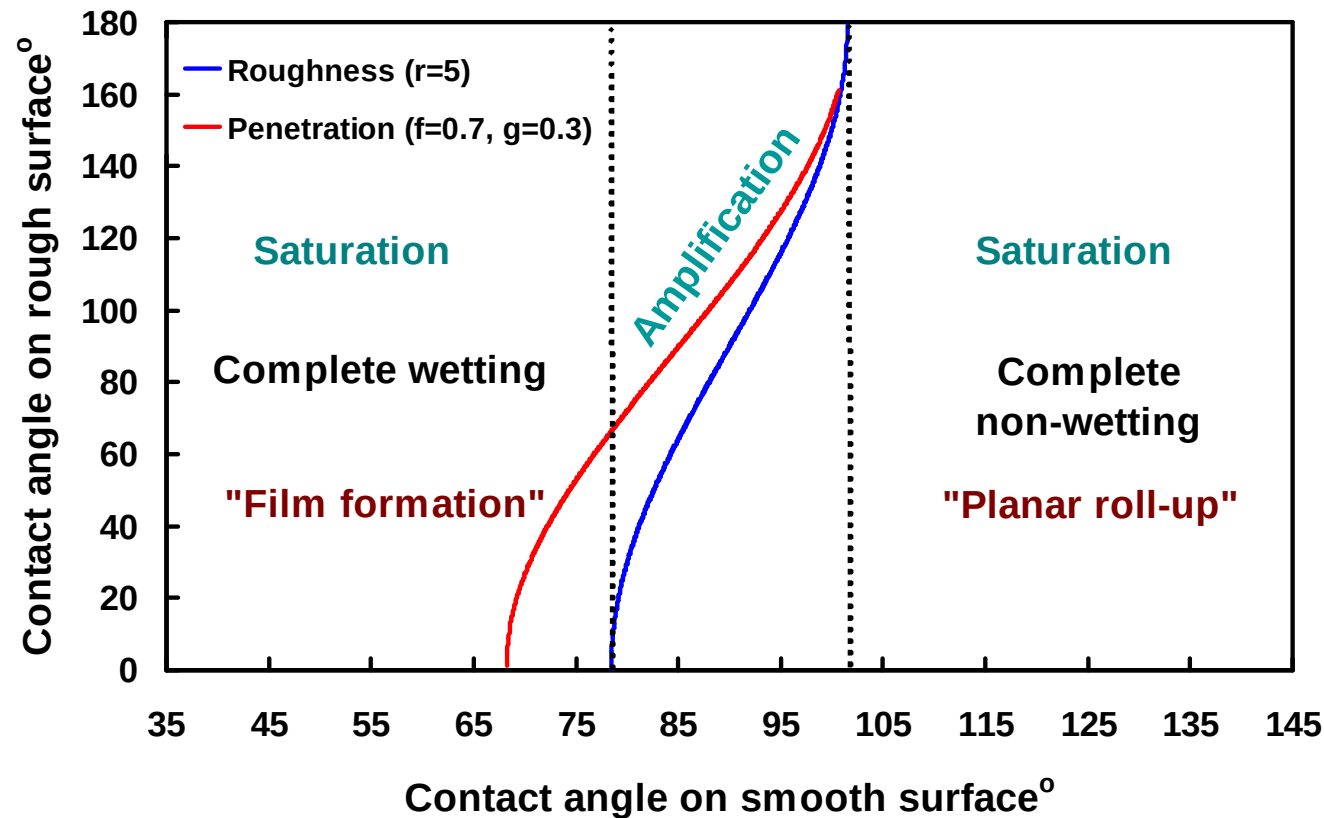
$$\Delta F = (\gamma_{SL} - \gamma_{SV})fr\Delta A + \gamma_{LV}g\Delta A + \gamma_{LV} \cos \theta \Delta A$$

Modified (Cassie Style) Eqn

$$\cos \theta_e^R = rf \cos \theta_e^S - g$$

$$f = \text{fraction of rough surface wet}$$

Effect of Topography - Equilibrium



Roughness/Topography

$\theta_e^s > \text{threshold}$

⇒ enhances hydrophobicity

$\theta_e^s < \text{threshold}$

⇒ enhances film formation

Super-wetting

Super-hydrophobic

⇒ equilibrium experiments

Super-wetting

⇒ dynamic experiments

Wenzel and “Driving Force”

Smooth Surface

Drop Equilibrium – Young’s Law

$$\Rightarrow \cos \theta_e^s = (\gamma_{SV} - \gamma_{SL}) / \gamma_{LV}$$

Drop Edge Speed Dynamics

$$\Rightarrow v_E \propto \theta \gamma_{LV} (\cos \theta_e^s - \cos \theta)$$

$$\Rightarrow v_E \propto \theta \gamma_{LV} (\theta^2 - \theta_e^{s2})$$

Rough Surface

Drop Equilibrium - Wenzel

$$\Rightarrow \cos \theta_e^R = r \cos \theta_e^s$$

Drop Edge Speed Dynamics

$$\Rightarrow v_E \propto \theta \gamma_{LV} (r \cos \theta_e^s - \cos \theta)$$

$$\Rightarrow v_E \propto \theta \gamma_{LV} ((r-1) + ((\theta^2 - r \theta_e^{s2})/2))$$

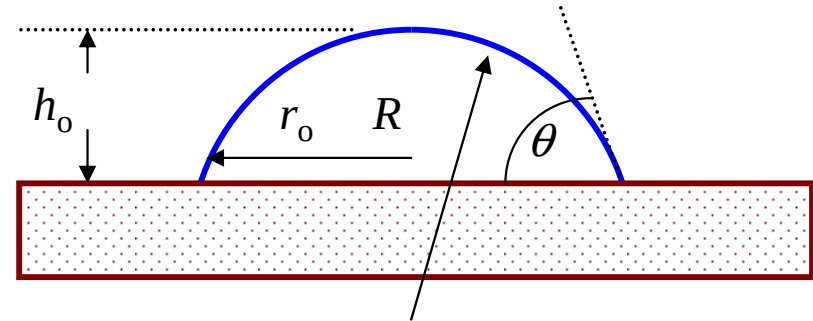
Prediction

Weak roughness or topographic patterning modifies edge speed:

$$v_E \propto \theta (\theta^2 - \theta_e^{s2}) \quad \text{changes towards} \quad v_E \propto \theta$$

Dynamics - Frenkel's Method

- Frenkel's Method
 - Hydrodynamic approach
 - Spherical cap droplet
 - Viscous dissipation



Rate of surface free energy change = Viscous dissipation

- Advantages of the Method
 - On smooth surfaces correct limit for θ_e small
 - Provides an edge speed-wide angle relation
 - Covers partial wetting case $\theta_e \neq 0^\circ$
- Limitations of the Method
 - Results are for non-volatile liquids
 - Assumes a spherical cap shape (size $< \kappa^{-1}$)

Edge Speed - Contact Angle Relation

- Surface Free Energy from Shape

Edge speed is $v_E = dr_o/dt$

Interfacial areas of spherical cap

Topography

$$\frac{dF}{dt} = 2\pi r_o \gamma_{LV} [\cos \theta - frI + g] v_E$$

$$I = (\gamma_{SV} - \gamma_{SL}) / \gamma_{LV} = \cos \theta_e^s$$

- Form of Dissipation

Use dimensional argument

Poiseuille flow to estimate k

$$\frac{dE_d}{dt} = \frac{k\eta v_E^2 r_o}{\tan(\theta/2)}$$

- Edge Speed - Contact Angle Relation

$$v_E = \left(\frac{2\pi\gamma_{LV}}{k\eta} \right) \tan(\theta/2) [fr \cos \theta_e^s - \cos \theta - g]$$

- Small Angle Case

$$v_E \propto \theta \left((fr - 1 - g) + (\theta^2 - fr \theta_e^{s2})/2 \right)$$

Hoffmann-de Gennes
when $fr=1$ and $g=0$

$$v_E \propto \theta (\theta^2 - \theta_e^{s2})$$

“Roughness” Modified Tanner’s Law

- Dynamics of θ

- Spherical cap shape at all times
- Volume of liquid conserved
- v_E converted to $d\theta/dt$

- Power Law for θ

- Complete wetting $\theta_e^s=0$
- Small angle approx
- Solve for time dep.

$$\frac{d\theta}{dt} \propto -\theta^{7/3} \left[2(fr - 1 - g) + \theta^2 \right]$$

Two arrows branch from the equation above to the following results:

$\theta = \frac{B_s}{(t + C_s)^{3/10}} \sim \frac{1}{t^{3/10}}$

Tanner’s Law
($fr=1, g=0$)

$\theta = \frac{A_R(fr - g - 1)}{(t + C_R)^{3/4}} \sim \frac{1}{t^{3/4}}$

**Topography
Modified**

Prediction

Weak roughness or topographic patterning modifies power law:
power law changes from -3/10 towards -3/4

Experimental Approach

- Lithographic Surface

- SU-8 Photoresist
- Circular Pillars

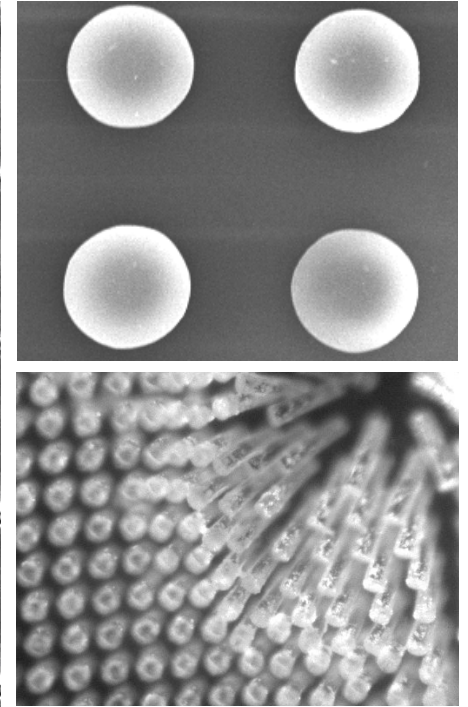
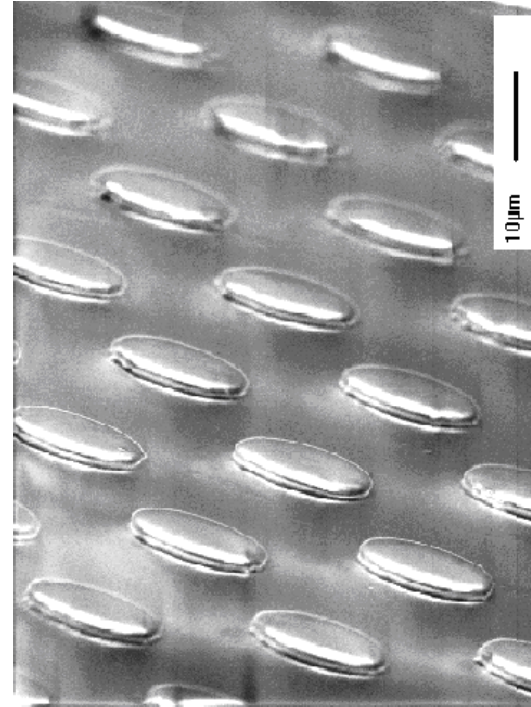
15 μm diameter

30 μm centre-centre

Square lattice

Vary height 0 to 30 μm

(bottom image is 4 μm pattern)



- Contact Angle Measurements

- Spreading/Wetting

PDMS Oil 10 000 cSt

- Super-hydrophobic

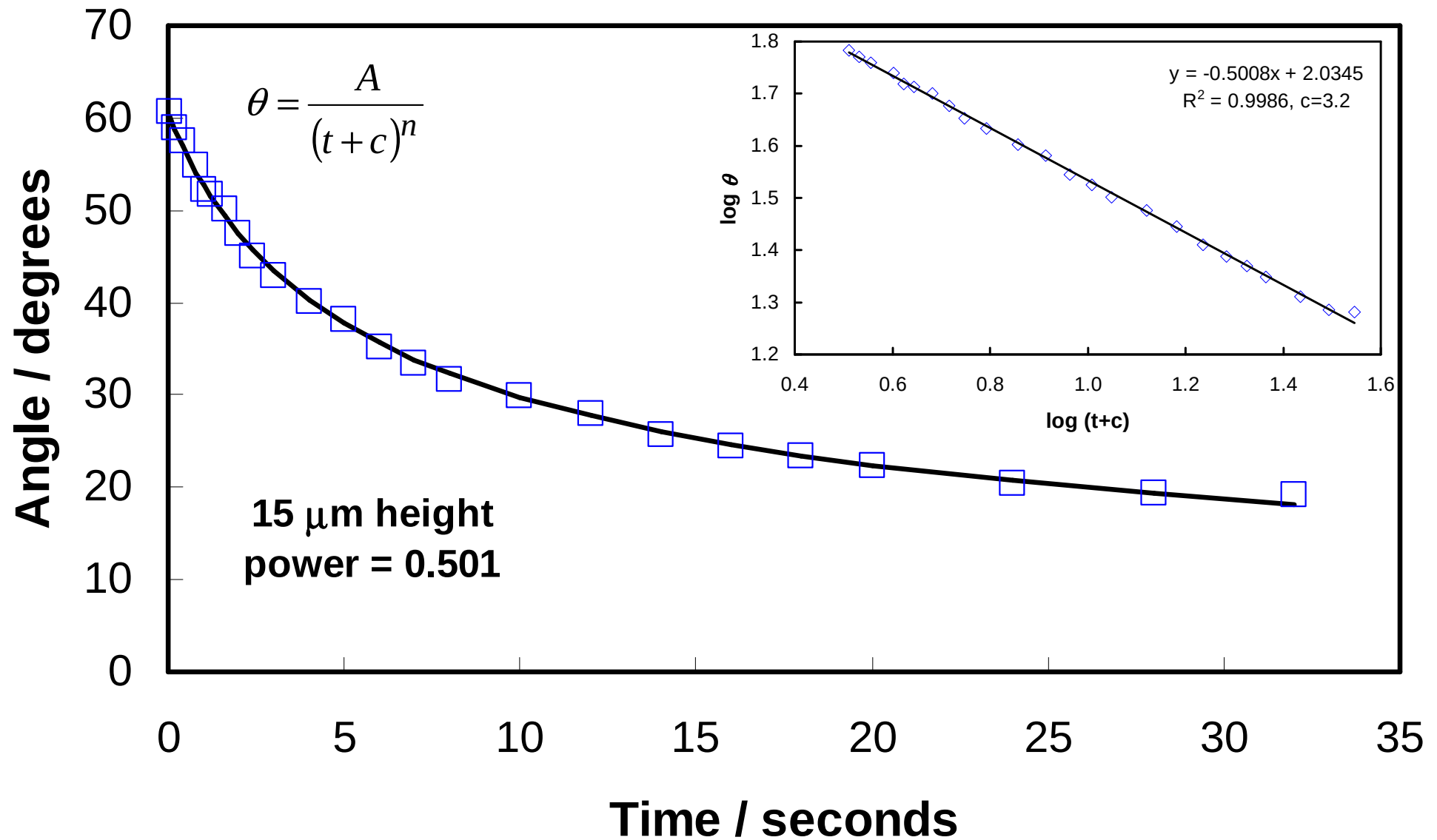
Hydrophobize surface

Equilibrium θ_e for water

Water Drop on Hydrophobized 20 μm

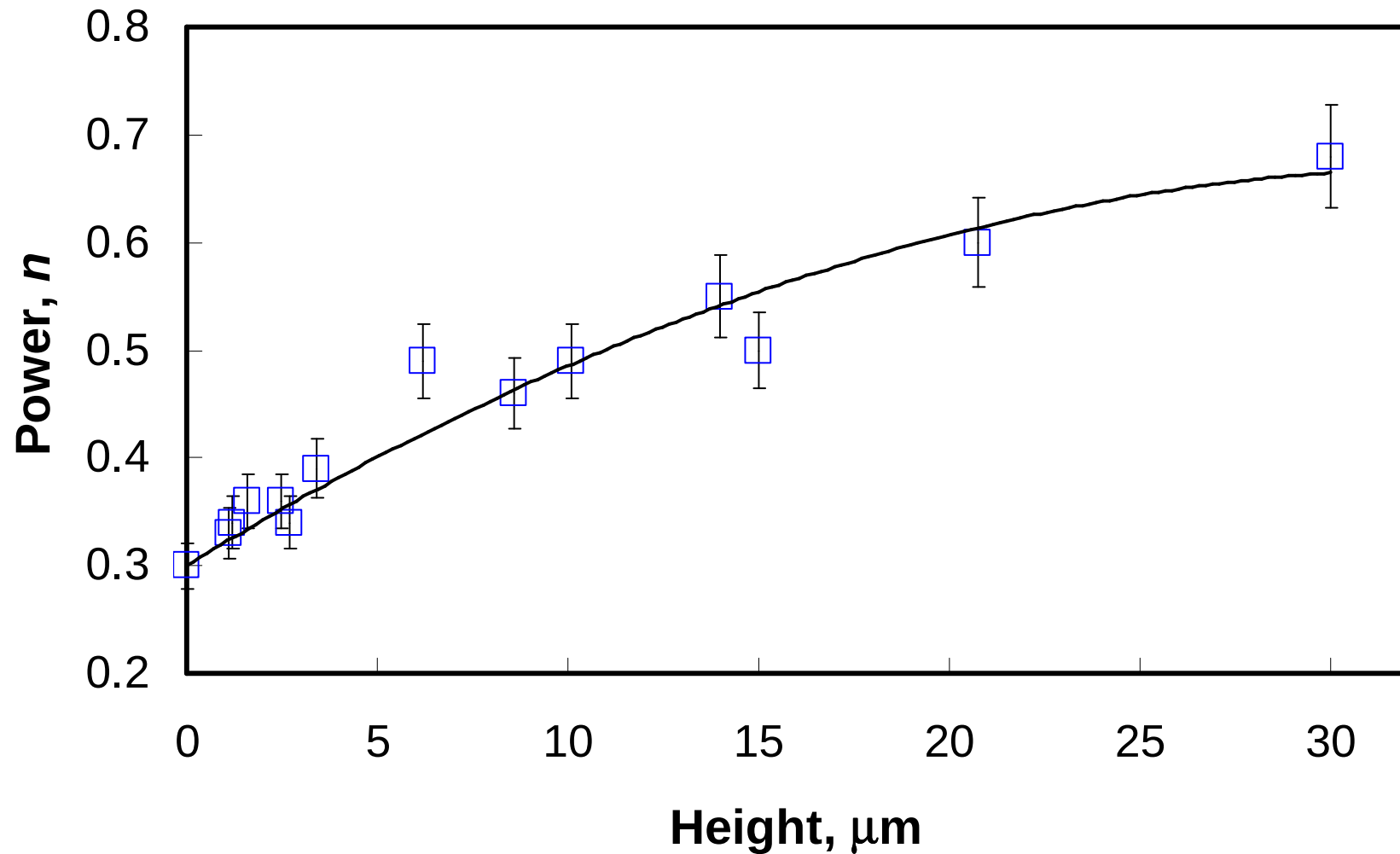


Dynamic Angle - Data and Fit



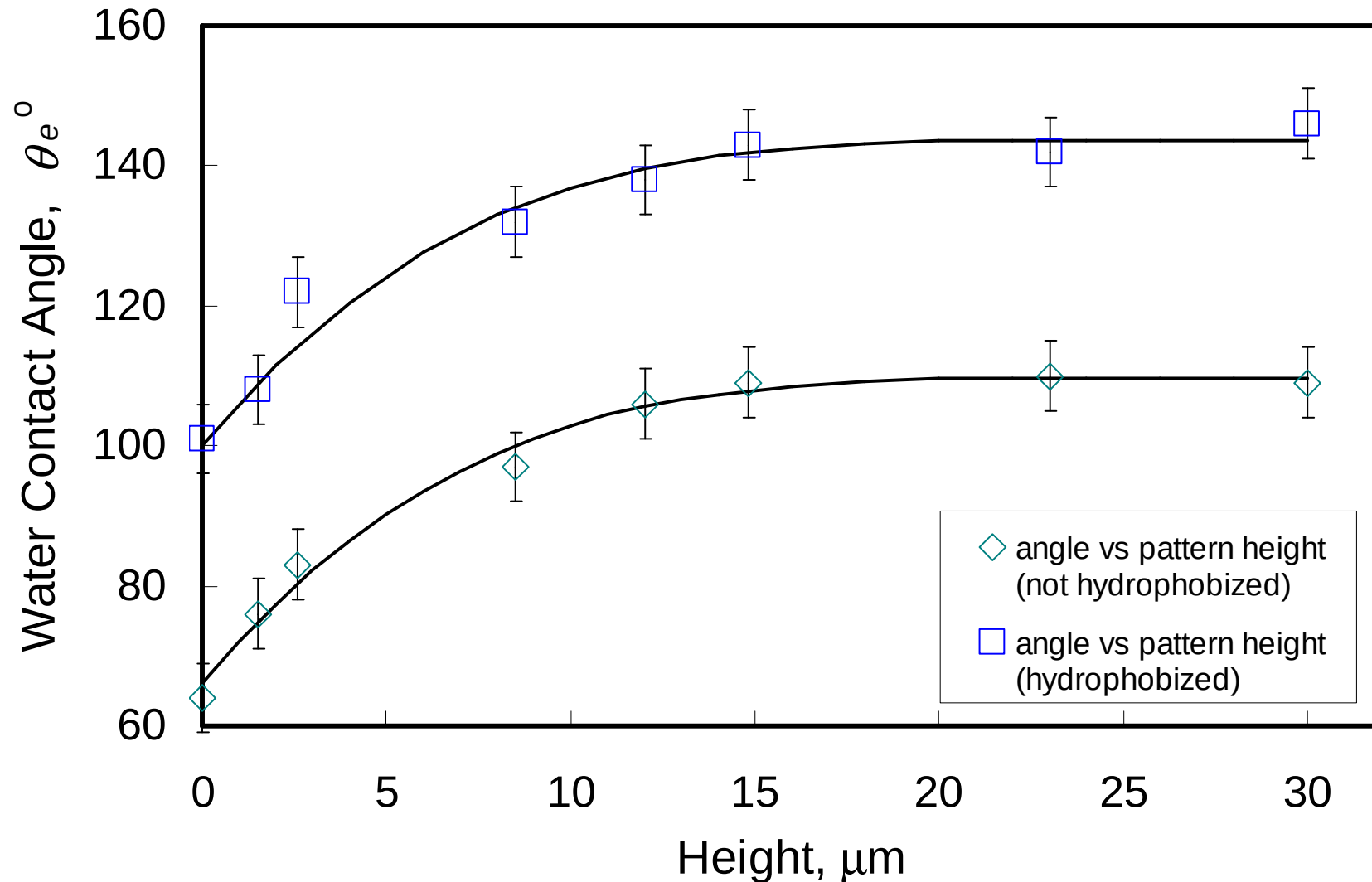
Super-wetting Data

- Exponents from Dynamics
 - PDMS oil and 0 to 30 μm heights



Super-hydrophobic Data

- Water Equilibrium Angles θ_e
 - untreated v hydrophobized patterned surfaces



Conclusions

Achievements

- Theory for Dynamics
Roughness version Tanner Law
- Controlled Surface Structure
Simple and systematic
- Super-Wetting
Dynamics $\Rightarrow$ super-wetting
- Hydrophobic Treatment
Equilib $\Rightarrow$ super-hydrophobic

Comments

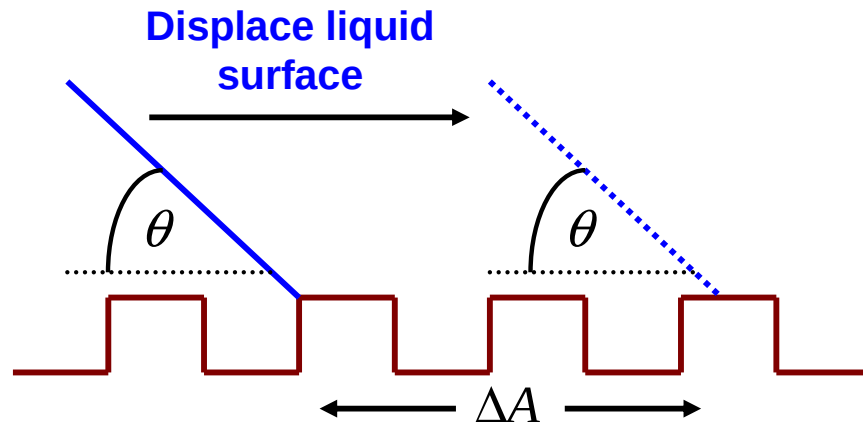
- Simplistic Theory
Dissipation/fast v slow directions
- Other Types of Surface Possible
Topographic structuring
- Dynamic Version of Cassie-Baxter
Pattern by chemical modification
- Foot and Precursor Films
Symmetry of film v drop

The End

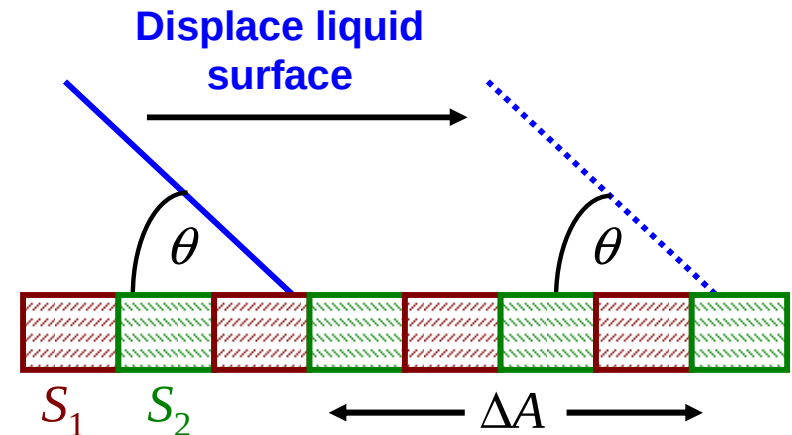
Additional Supporting Slides

Wetting and Topography

Surface Topography



Mixed Chemistry



Surface Free Energy Changes

$$\Delta F = (\gamma_{SL} - \gamma_{SV}) r \Delta A + \gamma_{LV} \cos \theta \Delta A$$

Wenzel's Equation

$$\cos \theta = r(\gamma_{SV} - \gamma_{SL}) / \gamma_{LV} = r \cos \theta_e^S$$

$$\Delta F = (\gamma_{SL}^1 - \gamma_{SV}^1) f \Delta A + (\gamma_{SL}^2 - \gamma_{SV}^2)(1-f) \Delta A + \gamma_{LV} \cos \theta \Delta A$$

Cassie's Equation

$$\cos \theta_e = f \cos \theta_1 + (1-f) \cos \theta_2$$

Chemically Heterogeneous Case

- Surface Free Energy from Shape

Edge speed is $v_E = dr_o/dt$

Interfacial areas of spherical cap

$$\left. \begin{array}{l} \text{Edge speed is } v_E = dr_o/dt \\ \text{Interfacial areas of spherical cap} \end{array} \right\} \frac{dF}{dt} = 2\pi r_o \gamma_{LV} [\cos \theta - fI_1 - (1-f)I_2] v_E$$

$$I = (\gamma_{SV} - \gamma_{SL}) / \gamma_{LV} = \cos \theta_e^s$$

- Form of Dissipation

Use dimensional argument

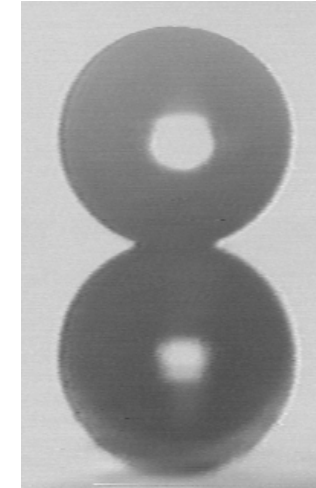
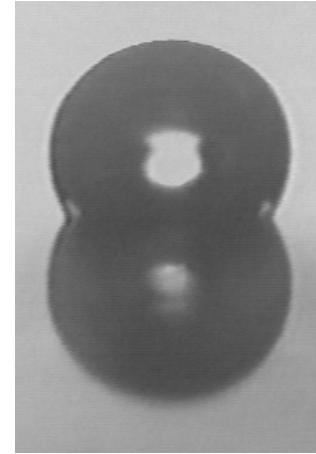
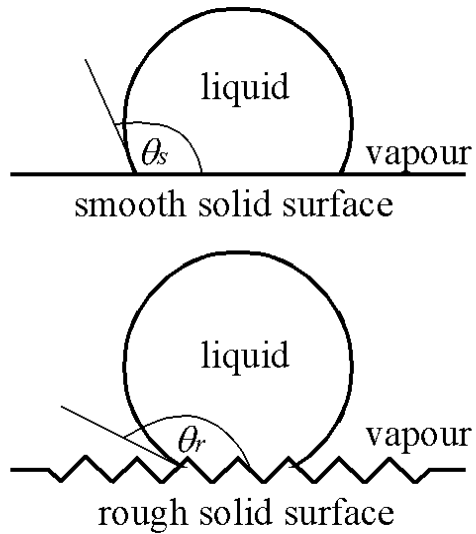
Poiseuille flow to estimate k

$$\left. \begin{array}{l} \text{Use dimensional argument} \\ \text{Poiseuille flow to estimate } k \end{array} \right\} \frac{dE_d}{dt} = \frac{k\eta v_E^2 r_o}{\tan(\theta/2)}$$

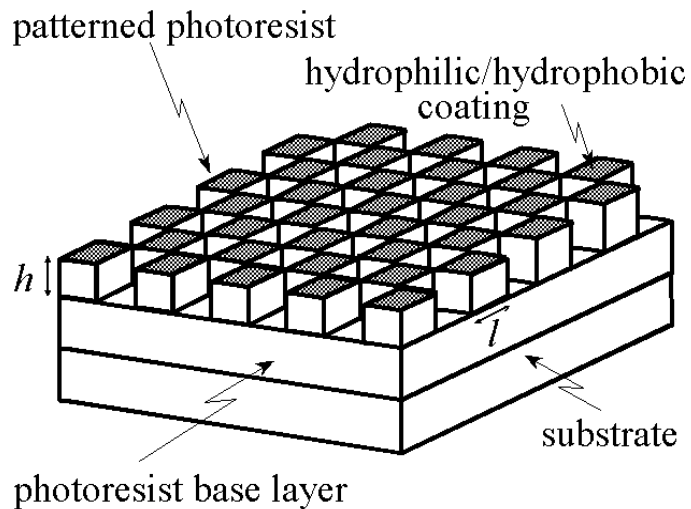
- $v_E - \theta$ Relation

$$v_E = \left(\frac{2\pi\gamma_{LV}}{k\eta} \right) \tan(\theta/2) [fI_1 + (1-f)I_2 - \cos \theta]$$

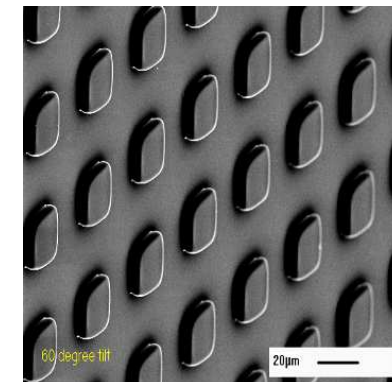
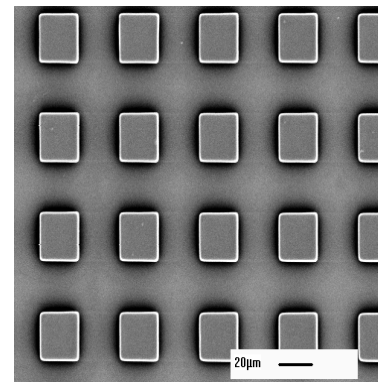
Super-Hydrophobic Surfaces



Lithographic Principle

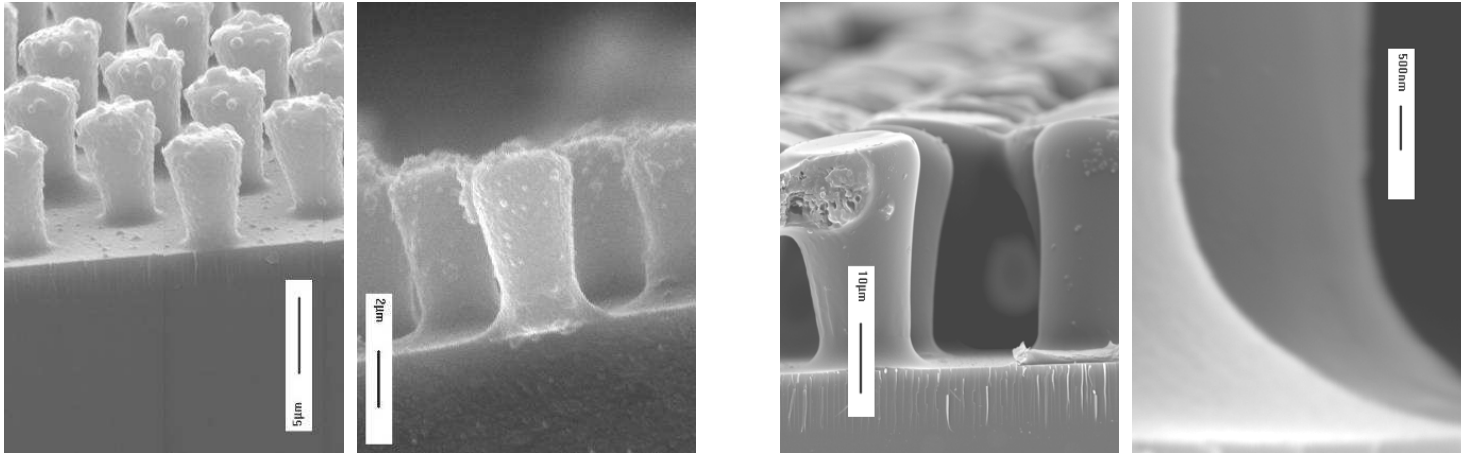


SEM Images

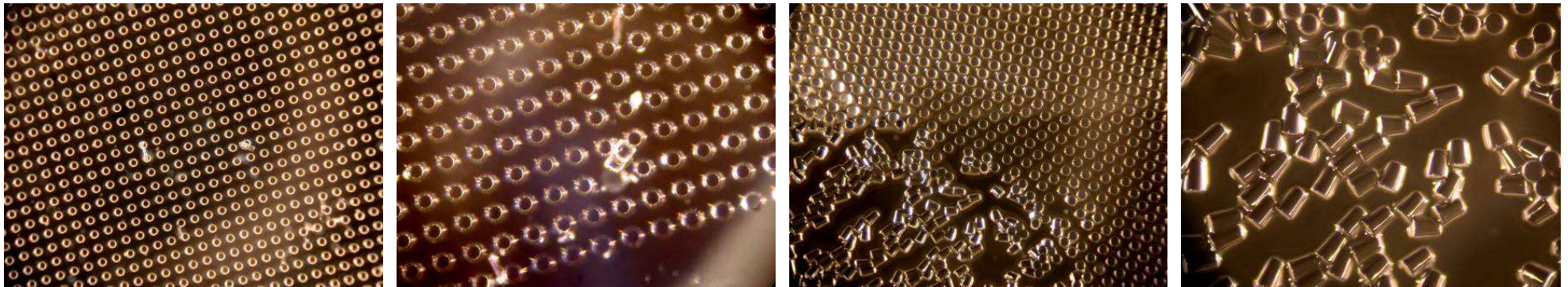


Additional Views of Pillars

- Coated SU-8 Circular Pillars
 - Spin @ 3000 rpm x 2 and no spin (incl. close up)



- Pillars - 20 μm Diameter by 40 μm (Samples a,b)



Views Pillars

- Lithographic Surface

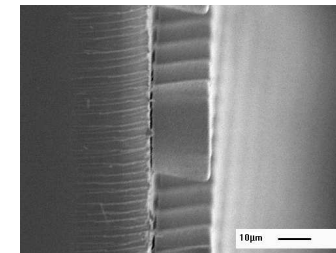
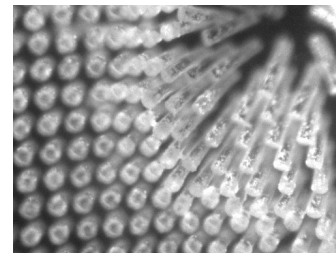
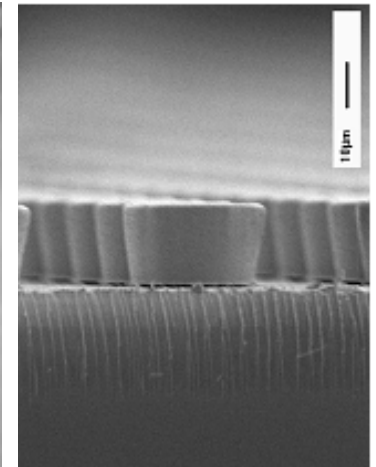
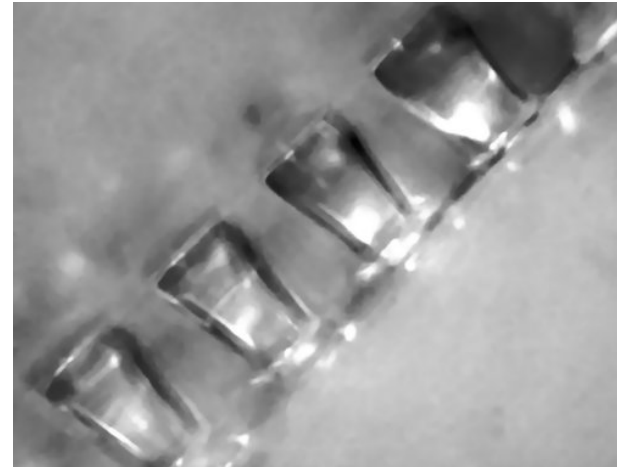
- SU-8 Photoresist

- Circular Pillars

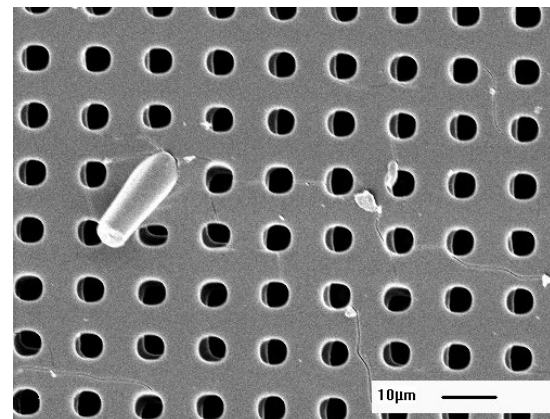
- 15 μm diameter

- 30 μm centre-centre

- Square lattice

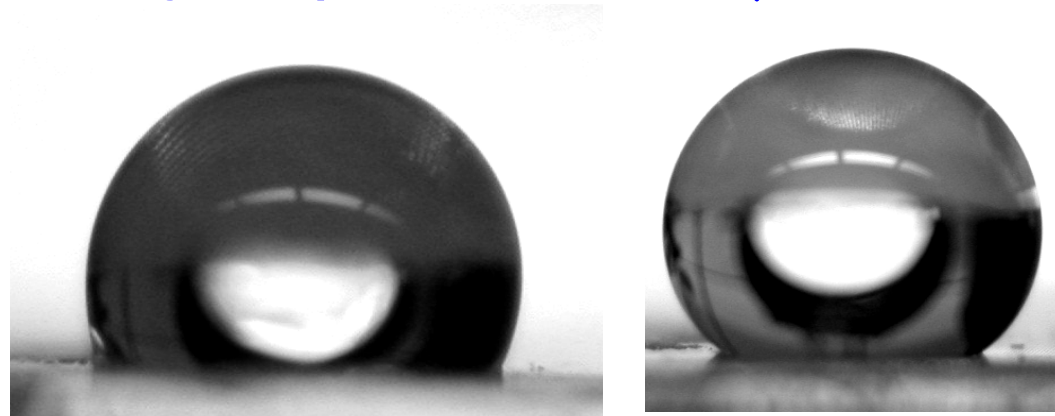


- 4 μm Diameter Pillars

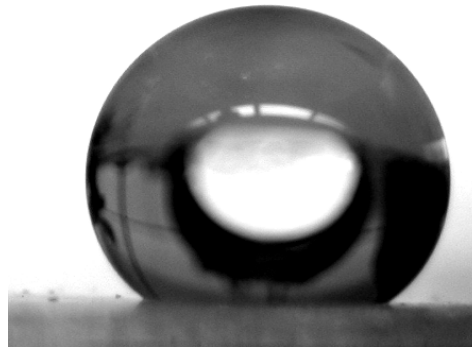


Hydrophobised Patterns of Pillars

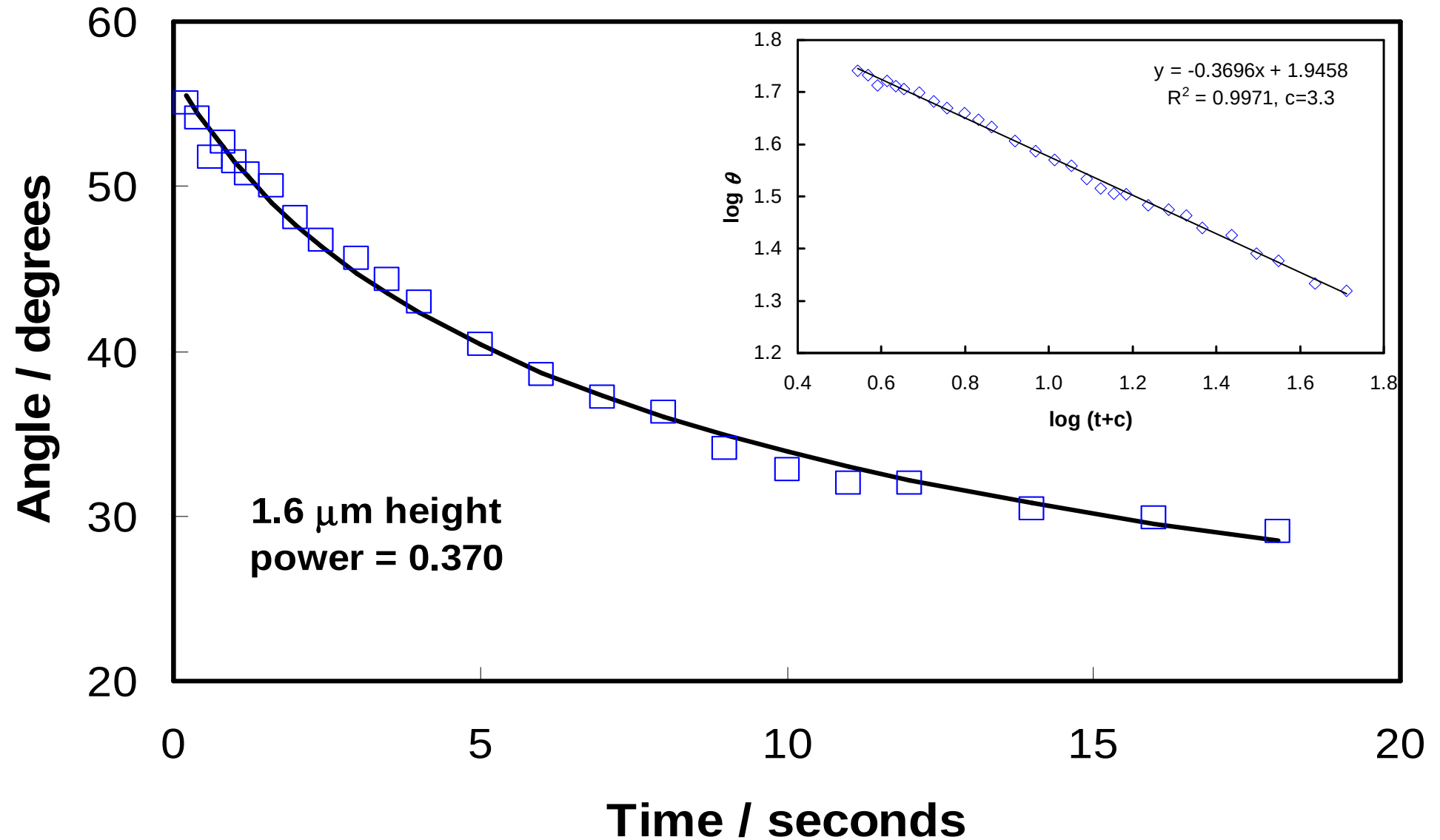
- Coated SU-8 Circular Pillars
 - Height is 30 μm , diameter is 15 μm and separation is 15 μm
- Bare and Hydrophobised 30 μm Pattern



- Hydrophobised 23 μm Pattern



Dynamic Angle - Data and Fit



Alternative Surfaces

Electrodeposited Surfaces

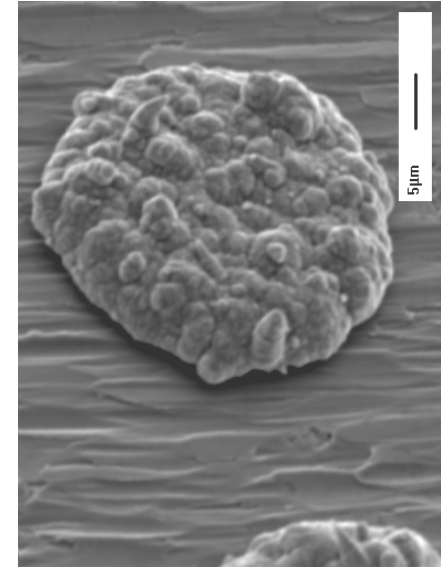
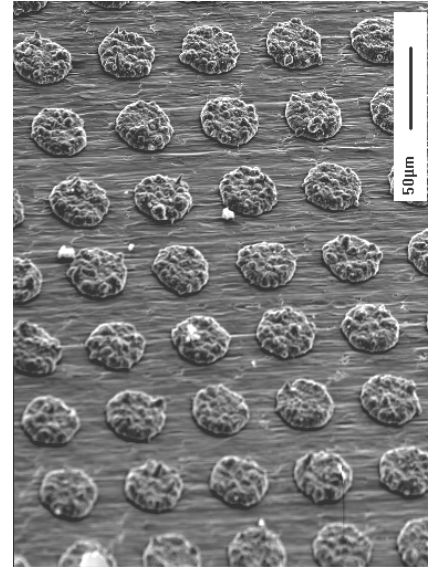
- Cu Deposited Surface

- Circular “Pads”

- 20 μm diameter

- 40 μm centre-centre

- Square lattice



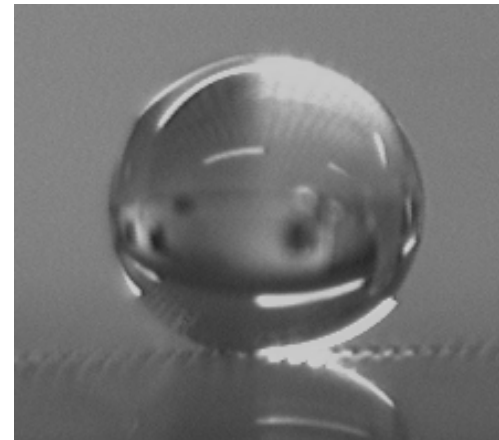
- Super-hydrophobicity

- Hydrophobize surface

- Gore-tex treatment

- Flutec treatment

Water Drop on Hydrophobized 20 μm



Copper Etched Surfaces

- Etched Copper
 - Chessboard pattern
 - 20 μm diameter

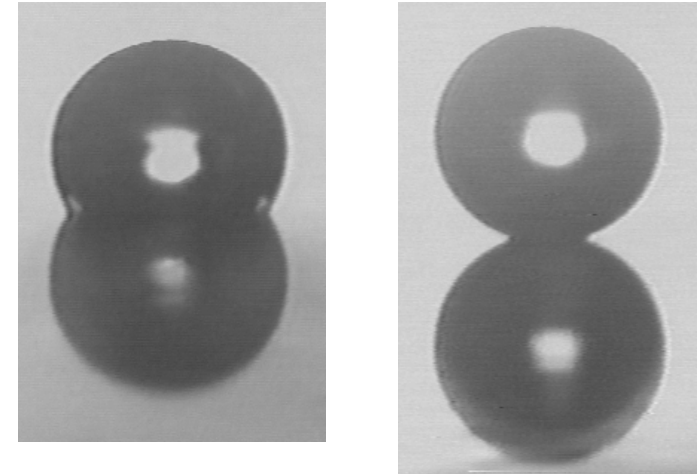


Fig 1. Enhancement of hydrophobicity.

- Evaporation
 - Squares = data on a substrate where the coating is resistant to damage due to exposure to the water.
 - Crosses = data where the hydrophobic coating is effectively removed during evap.

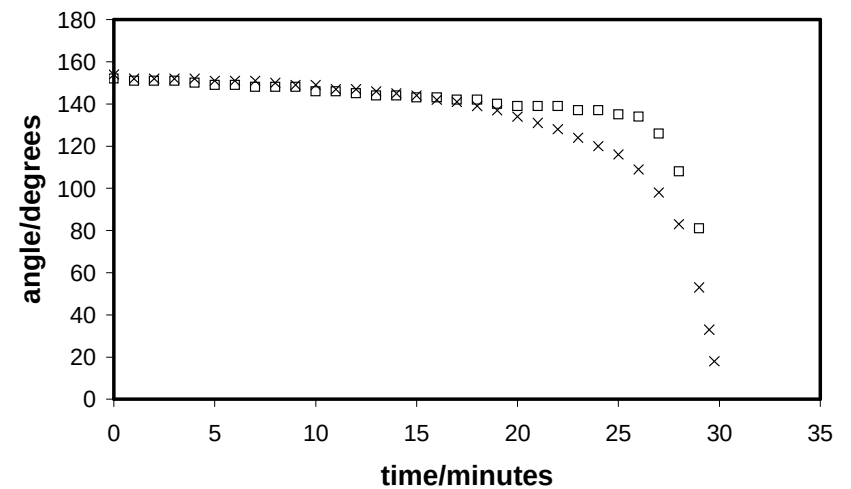


Fig. 2 Evaporation sequences.

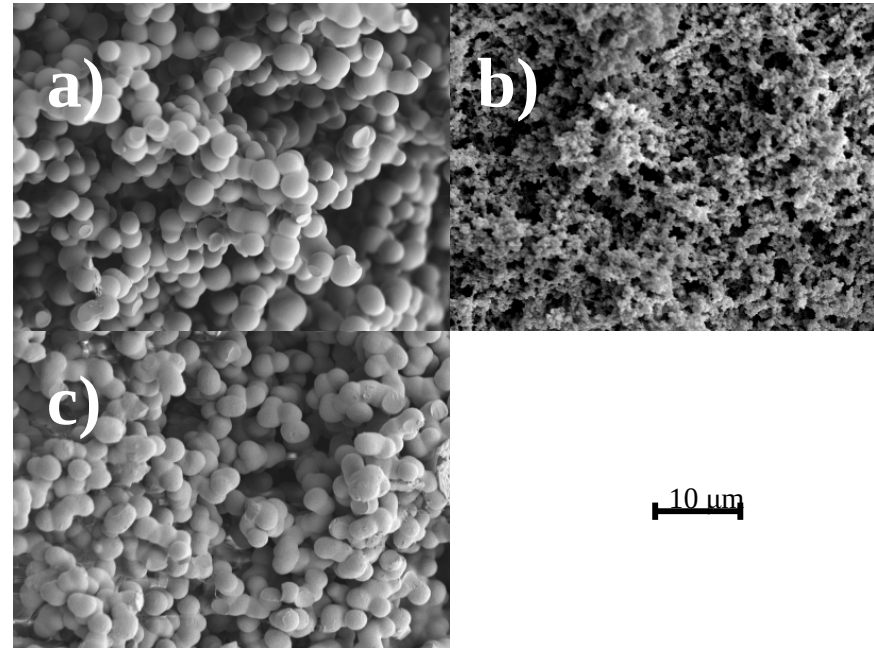
Sol-Gel Surfaces

- Phase-Separation

- Control via chemistry

- nm to 20 μm pores

- a) MTEOS with 1.1 M ammonia, heated to 300°C;
 - b) MTEOS with 2.2 M ammonia, heated to 300°C;
 - c) PTEOS/MTEOS with 22 M ammonia, heated to 300°C



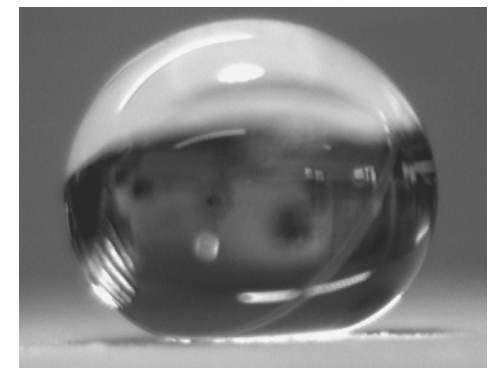
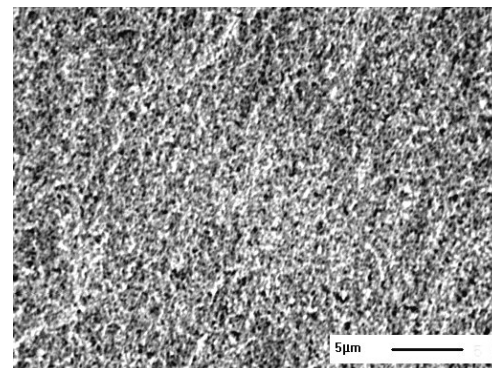
- Super-hydrophobicity

- no need to hydrophobize

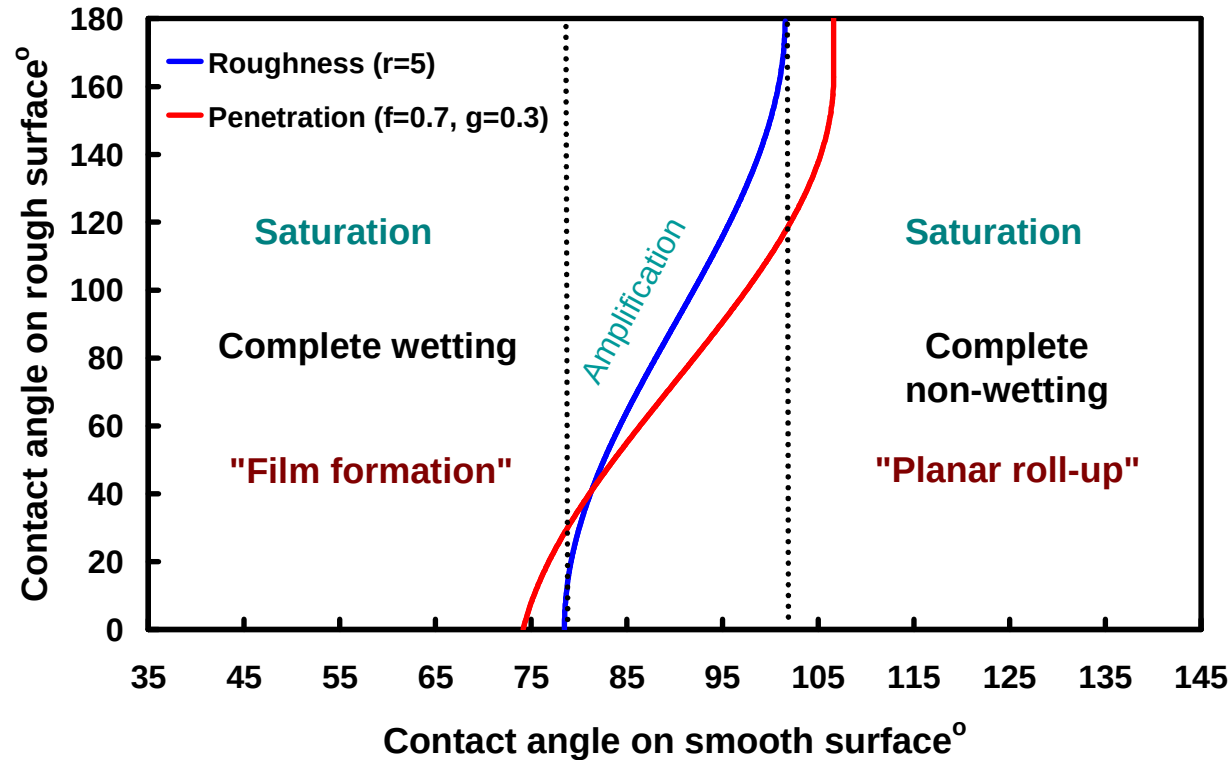
- heating converts surface

- Completely imbibes water

- Chemical treatment regains super-hydrophobicity



Effect of Topography - Equilibrium



Roughness/Topography

$\theta_e^s > \text{threshold}$

$\Rightarrow$ enhances hydrophobicity

$\theta_e^s < \text{threshold}$

$\Rightarrow$ enhances film formation

Super-wetting

Super-hydrophobic

$\Rightarrow$ equilibrium experiments

Super-wetting

$\Rightarrow$ dynamic experiments